

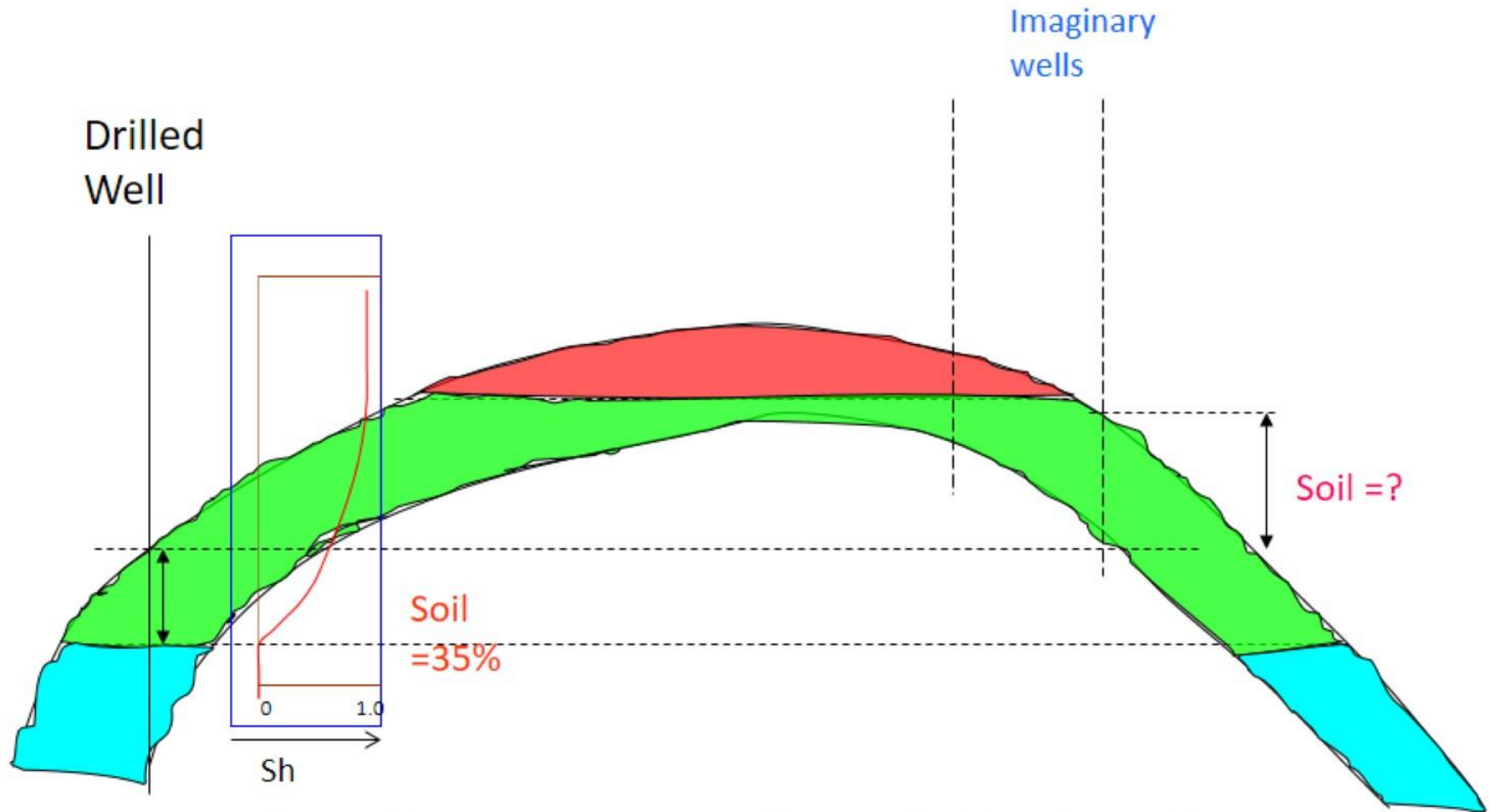
Saturation-Height Function

Leong Hoon Yoong

Saturation-Height Function

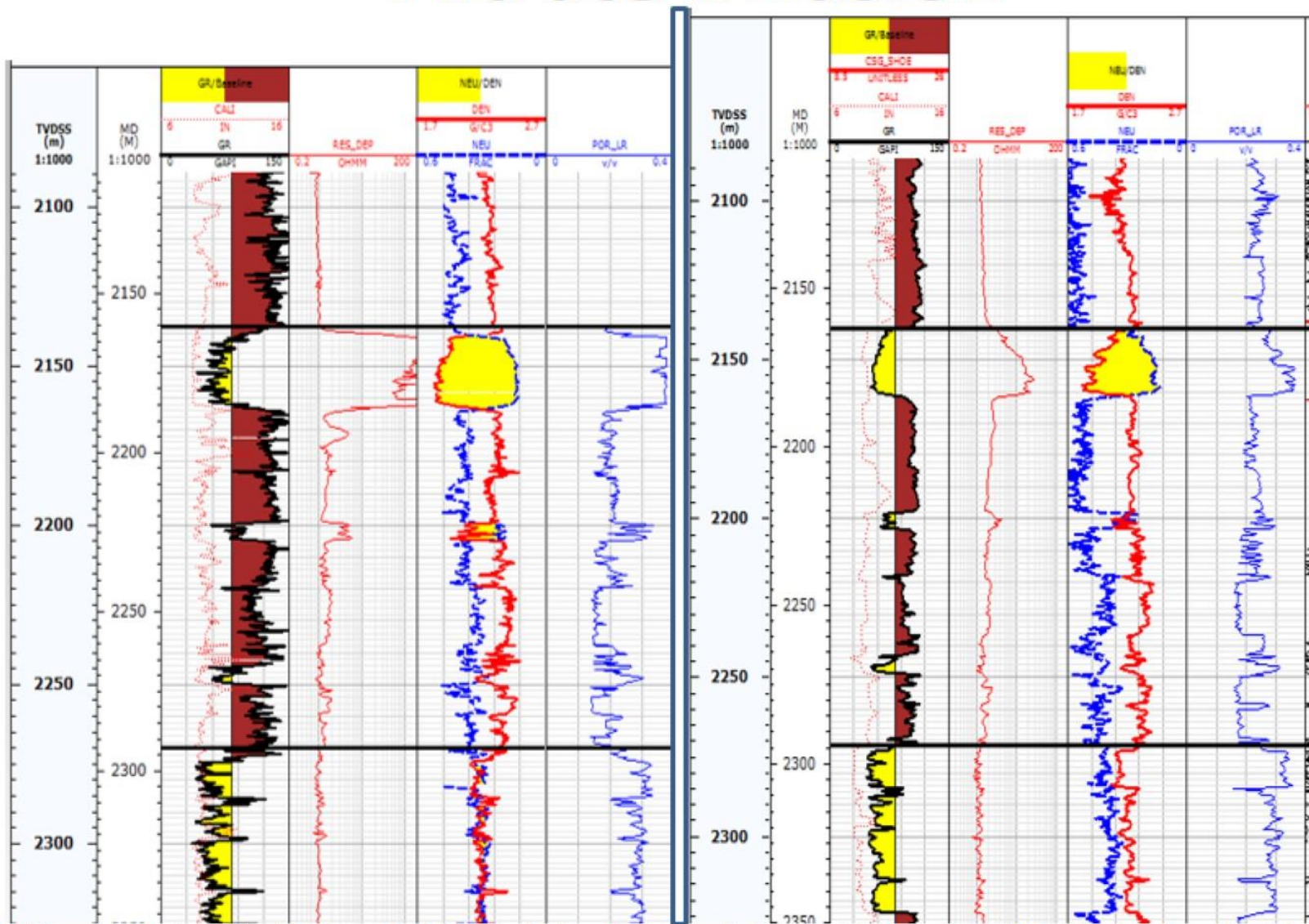
Why use saturation-Height Function?

Why not use log-derived saturation?



Should we use a well result (S_w) as the average S_w for the whole reservoir?

Filtrate Invasion



LWD resistivity in original hole reads 10 times higher than the wireline resistivity in the sidetracked well on the right due to invasion effect. gas saturation=91%PU for the original hole and 71%PU for the sidetrack hole.

Who use saturation-height function

- Geologist uses it to generate GIP or OIP in his static model
- The result of static model is passed to Reservoir Engineer for the starting point of his dynamic modelling (history matching).

Capillary pressure and Buoyancy
force in hydrocarbon charge into
the reservoir

Capillary force and capillary pressure

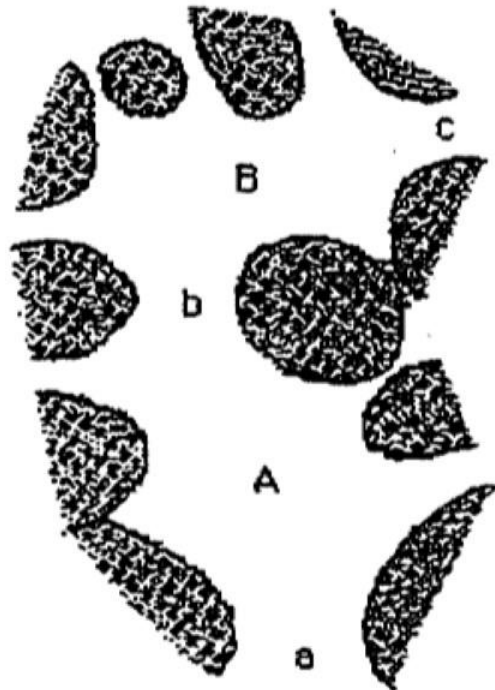


Figure 1.

Cross section of a pore.

The water in the pore space is at a hydrostatic pressure. The larger pores (A and B) are connected by smaller diameter pore throats (a and b); pore throat c leads to the next pore.

As numerical values for parameters are easier to visualise, the pore throats are given realistic diameters which will be used in the examples:

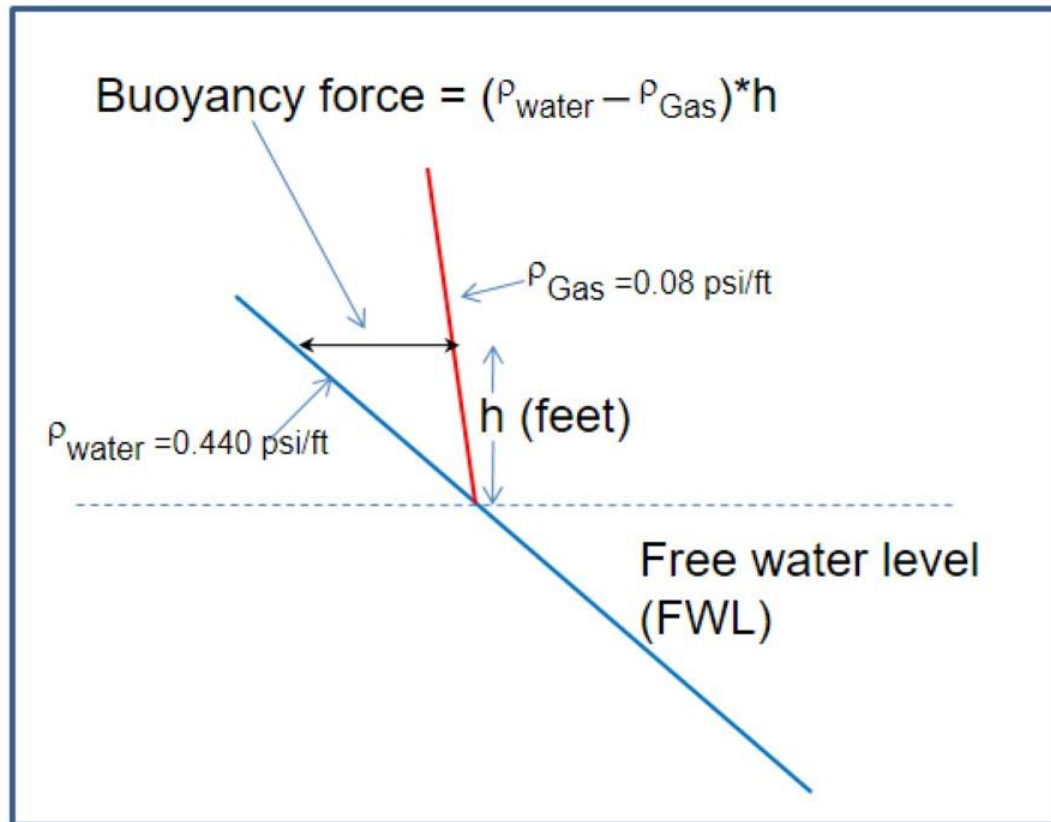
- a = 4 μm,*
- b = 3 μm,*
- c = 2 μm.*

The capillary pressure holding the water in the pore = P_c

$$P_c = 2 \sigma \cos\theta / r \dots\dots\dots(1)$$

Where σ is the interfacial tension between gas or oil and water,
 θ is the contact angle between the wetting phase (water) and the rock,
 and r is the radius of the pore throat

Buoyancy force



Charging of reservoir



$$\Delta\rho \cdot g \cdot h < 2\sigma \cos\theta/r$$



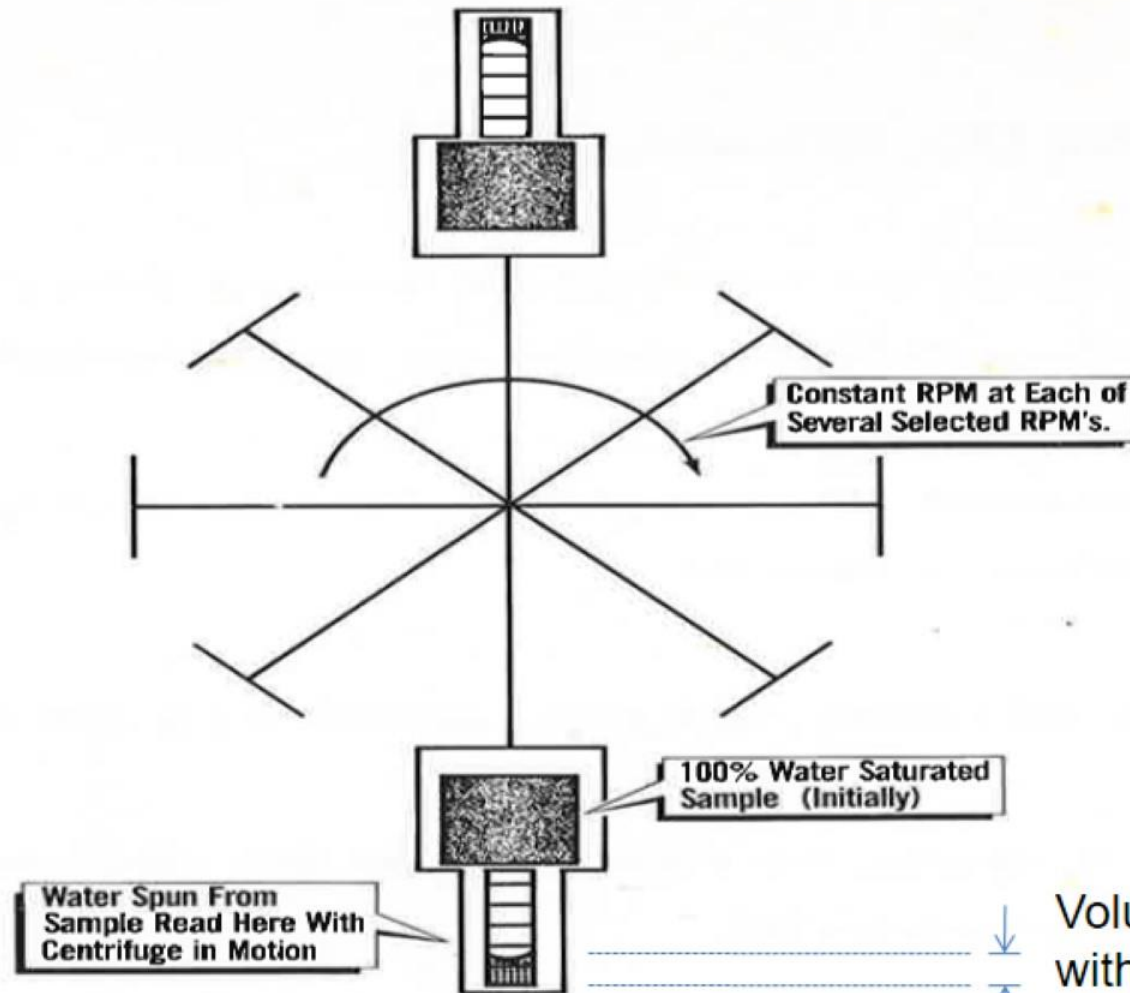
$$\Delta\rho \cdot g \cdot h \geq 2\sigma \cos\theta/r$$

History repeated in the Laboratory

Capillary pressure test

Capillary Pressure Test

Acceleration = $r\omega^2$
Where r is the rotational radius, and ω is the angular velocity in revolution per minute



Centrifugal Apparatus (Drainage)

Volume of brine can be read with a stroboscope (using photo or the eye)

Typical Capillary Pressure Result

Microsoft Excel 2010 interface showing a spreadsheet titled "Typical Cap. Pressure result [Compatibility Mode]". The spreadsheet contains the following data:

Page : 4 - 1
File : SCM00007

SUMMARY OF CAPILLARY PRESSURE RESULTS
Centrifuge Method - Ambient Condition

Fluid System : Air - Water (Drainage)
Test Method : High Speed Centrifuge
Conditions : Ambient

Sample ID	Depth ft	Klinkenberg Permeability md	Permeability to air (est.) md	Porosity %	Pressure, psi :											
					0	1	2	5	10	25	50	100	200	350		
Net Overburden (800 psi)																
Inlet-Face Water Saturation																
% Pore Volume																
196A	6812.6	685.	690.	22.6	100.0	68.2	49.8	33.5	25.3	18.1	14.5	12.1	10.5	9.6		
91A	6693.0	332.	337.	22.0	100.0	87.3	71.7	35.6	27.1	21.7	18.8	16.5	14.5	12.8		
75A	6675.5	50.	54.	21.3	100.0	85.5	73.8	56.0	42.9	28.5	20.8	16.2	13.5	11.9		
89A	6690.8	211.	218.	21.2	100.0	94.2	73.6	43.3	29.4	23.2	20.9	19.2	17.4	15.0		
93A	6695.1	297.	305.	20.9	100.0	76.1	54.2	35.0	25.8	18.3	15.0	12.5	10.3	7.7		
105A	6708.3	90.6	95.4	20.1	100.0	100.0	81.6	53.6	41.2	31.1	26.2	22.9	20.6	19.3		
23A	6618.2	4.7	5.8	19.5	100.0	100.0	100.0	95.9	82.9	55.2	45.1	37.4	32.9	31.3		
248A	6870.3	109.1	114.3	19.1	100.0	92.1	68.2	47.0	36.4	26.9	22.1	18.7	16.3	14.9		
242A	6864.0	44.0	48.2	19.0	100.0	81.8	68.6	48.3	35.3	24.4	19.9	17.2	15.6	14.8		
157A	6768.6	18.6	21.0	18.3	100.0	100.0	97.6	81.4	66.6	47.9	38.3	33.0	29.8	28.1		
123A	6731.3	63.5	67.5	17.8	100.0	99.9	89.0	56.7	41.7	33.6	29.2	25.7	23.1	21.3		
132A	6741.1	33.9	37.2	16.8	100.0	100.0	93.6	65.5	51.0	37.4	29.8	24.0	19.5	16.8		
319A	7448.7	24.2	26.8	16.4	100.0	100.0	94.3	69.1	53.9	39.3	31.8	26.2	21.9	18.3		
322A	7452.3	27.81	30.60	16.4	100.0	100.0	88.1	68.1	53.8	41.2	34.3	28.6	23.8	20.5		
171A	6783.8	5.37	6.41	16.1	100.0	100.0	100.0	80.8	64.7	49.0	40.5	34.4	30.4	28.3		

Typical Interfacial Tension and contact angle constants

<u>System</u>	<u>θ Contact Angle</u>	<u>Cosine Contact θ</u>	<u>T Interfacial Tension</u>	<u>T Cosine θ</u>
Laboratory				
Air-water	0	1.0	72	72
Oil-water	30	0.866	48	42
Air-mercury	140	0.765	480	367
Air-oil	0	1.0	24	24
Reservoir				
Water-oil	30	0.866	30	26
Water-gas	0	1.0	50*	50

* Pressure and temperature dependent. Reasonable value to depth of 5000 feet.

“normalized” Capillary pressure, PC_IFT

- $\frac{PC_{A-Hg}}{(T\cos\theta)_{A-Hg}} = \frac{PC_{A-B}}{(T\cos\theta)_{A-B}} = \text{Constant}$
- $PC_IFT = (PC_{\text{system } x}) / (T\cos\theta)_{\text{system } x}$

Conversion of Air-Mercury (A-Hg) Capillary Pressure Data to Air-Brine (A-B) Data

- $$\begin{aligned} PC_{A-Hg} &= PC_{A-B} * (T \cos \theta)_{A-Hg} / (T \cos \theta)_{A-B} \\ &= PC_{A-B} * 367 / 72 \\ &= 5.1 * PC_{A-B} \end{aligned}$$

Leverett-J function & RQI

$$J = \frac{P_c}{\sigma \cdot \cos\theta} \cdot \sqrt{\frac{k}{\phi}}$$

$$J = 0.2166 \cdot P_c \cdot \text{SQRT}(k/\phi)$$

P_c in psi, k in mD and ϕ in fraction

$$\text{RQI} = 0.0314 \sqrt{\frac{k}{\phi}}$$

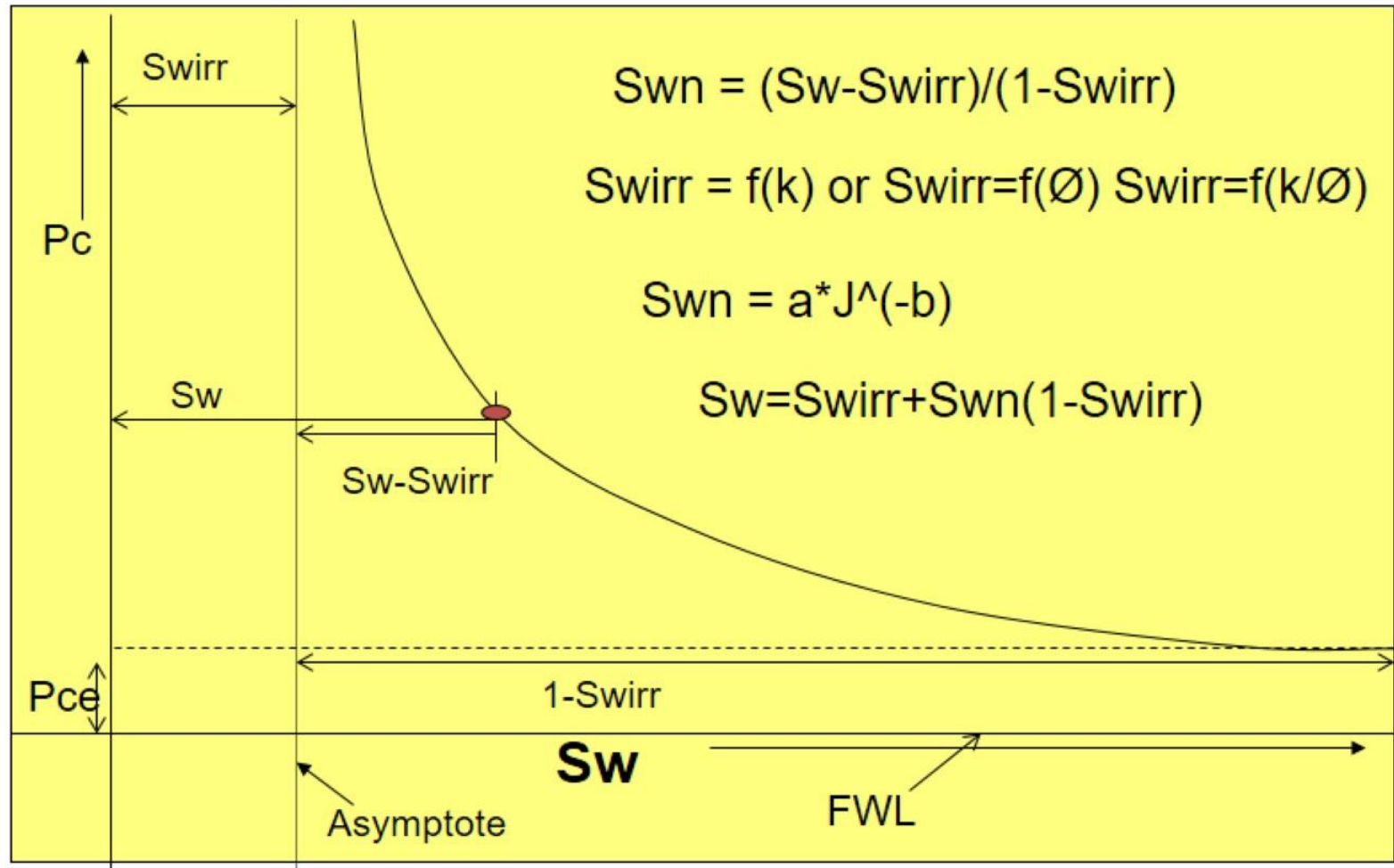
$\sigma \cos\phi = 72$ dynes/cm

		Pressure,	psi :												
			0	1	2	5	10	25	50	100	200	350			
Sample ID	Depth m	Net Overburden (800 psi)			Leverett-J								SQRT(k/Phi)	RQI	
		Klinkenberg Permeability md	Permeability to air (est.) md	Porosity %	% Pore Volume										
196A	2076.47	685.	690.	22.6									55.06	1.73	
91A	2040.02	332.	337.	22.0									38.82	1.22	
75A	2034.68	49.8	54.4	21.3									15.29	0.48	
89A	2039.36	211.	218.	21.2									31.56	0.99	
93A	2040.68	297.	305.	20.9									37.73	1.18	
105A	2044.70	90.6	95.4	20.1									21.23	0.67	
23A	2017.24	4.70	5.80	19.5									4.91	0.15	
248A	2094.07	109.	114.	19.1									23.90	0.75	
242A	2092.16	44.0	48.2	19.0									15.22	0.48	
157A	2063.06	18.6	21.0	18.3									10.08	0.32	
123A	2051.71	63.5	67.5	17.8									18.89	0.59	
132A	2054.70	33.9	37.2	16.8									14.20	0.45	
319A	2270.35	24.2	26.8	16.4									12.14	0.38	
322A	2271.45	27.8	30.6	16.4									13.02	0.41	
171A	2067.69	5.37	6.41	16.1									5.78	0.18	

Calculated J values

		Pressure, psi :			0	1	2	5	10	25	50	100	200	350		
		HAFWL				2.91545	5.8309	14.5773	29.1545	72.8863	145.773	291.5451895	583.09	1020.40816		
Sample ID	Depth m	Net Overburden (800 psi)			Leverette J										SQRT(k/Phi)	RQI
		Klinkenberg Permeability md	Permeability to air (est.) md	Porosity frac												
196A	2076.47	685.	690.	0.226	0.000	0.166	0.331	0.828	1.656	4.141	8.282	16.565	33.129	57.977	55.063	1.729
91A	2040.02	332.	337.	0.220	0.000	0.117	0.234	0.584	1.168	2.920	5.840	11.679	23.358	40.877	38.823	1.219
75A	2034.68	49.8	54.4	0.213	0.000	0.046	0.092	0.230	0.460	1.150	2.300	4.599	9.198	16.097	15.288	0.480
89A	2039.36	211.	218.	0.212	0.000	0.095	0.190	0.475	0.950	2.374	4.748	9.496	18.991	33.235	31.564	0.991
93A	2040.68	297.	305.	0.209	0.000	0.113	0.227	0.567	1.135	2.837	5.675	11.349	22.698	39.722	37.725	1.185
105A	2044.70	90.6	95.4	0.201	0.000	0.064	0.128	0.319	0.639	1.597	3.194	6.388	12.776	22.358	21.235	0.667
23A	2017.24	4.70	5.80	0.195	0.000	0.015	0.030	0.074	0.148	0.369	0.739	1.477	2.955	5.171	4.911	0.154
248A	2094.07	109.	114.	0.191	0.000	0.072	0.144	0.359	0.719	1.797	3.594	7.189	14.377	25.160	23.896	0.750
242A	2092.16	44.0	48.2	0.190	0.000	0.046	0.092	0.229	0.458	1.144	2.289	4.578	9.155	16.022	15.217	0.478
157A	2063.06	18.6	21.0	0.183	0.000	0.030	0.061	0.152	0.303	0.758	1.516	3.033	6.065	10.614	10.081	0.317
123A	2051.71	63.5	67.5	0.178	0.000	0.057	0.114	0.284	0.568	1.421	2.842	5.684	11.367	19.893	18.893	0.593
132A	2054.70	33.9	37.2	0.168	0.000	0.043	0.085	0.214	0.427	1.068	2.136	4.271	8.542	14.949	14.198	0.446
171A	2067.69	5.4	6.4	0.161	0.000	0.017	0.035	0.087	0.174	0.435	0.869	1.738	3.476	6.083	5.778	0.181
319A	2270.35	24.2	26.8	0.164	0.000	0.037	0.073	0.183	0.365	0.913	1.826	3.652	7.305	12.784	12.141	0.381
322A	2271.45	27.8	30.6	0.164	0.000	0.039	0.078	0.196	0.392	0.979	1.959	3.917	7.835	13.711	13.022	0.409

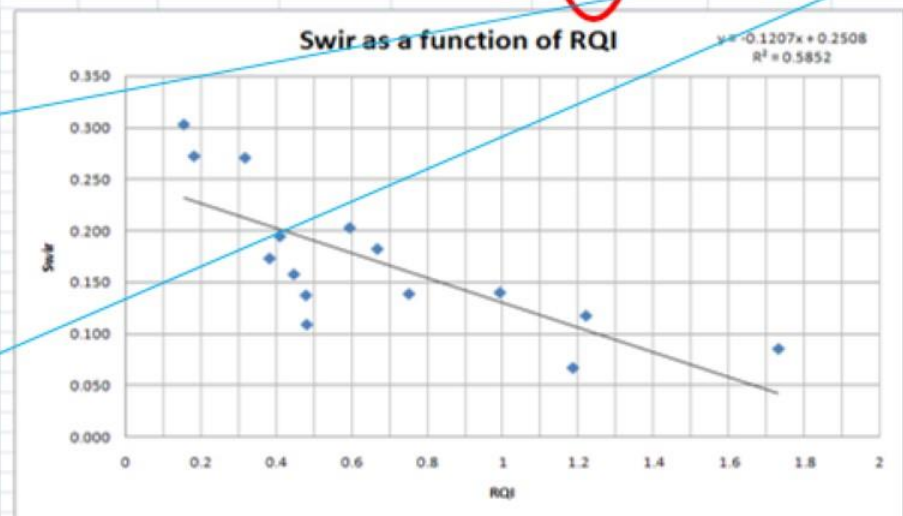
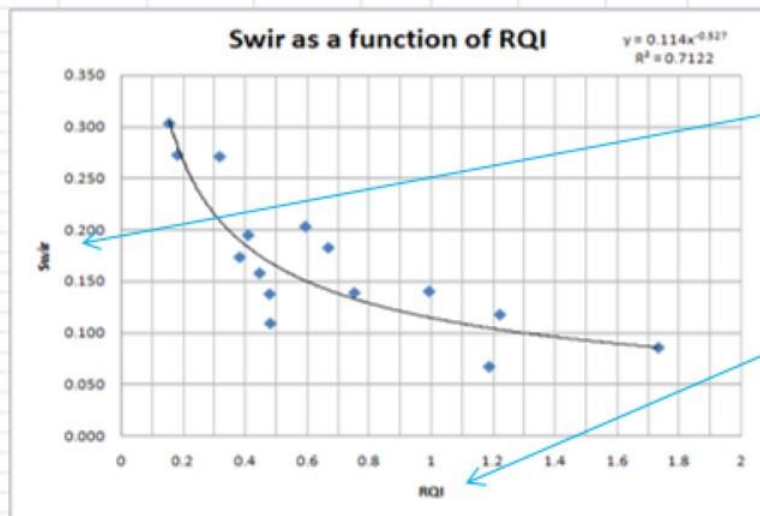
Brooks and Corey Method



Swirr

Sw at 350 psi -0.01

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	
9																				
10				Pressure,		psi :	0	1	2	5	10	25	50	100	200	350				
11																				
12				Net Overburden (800 psi)																
13	Sample	Depth	Klinkenberg	Permeability																
14	ID		Permeability	to air (est.)	Porosity															
15																				
16		m	md	md	frac												Sw _{irr}	SQRT(k/Phi)	RQI	
17	196A	2076.47	685.	690.	0.226	1.000	0.682	0.498	0.335	0.253	0.181	0.145	0.121	0.105	0.096	0.086	55.063	1.728971		
18	91A	2040.02	332.	337.	0.220	1.000	0.873	0.717	0.356	0.271	0.217	0.188	0.165	0.145	0.128	0.118	38.823	1.219032		
19	93A	2040.68	297.	305.	0.209	1.000	0.761	0.542	0.350	0.258	0.183	0.150	0.125	0.103	0.077	0.067	37.725	1.184572		
20	89A	2039.36	211.	218.	0.212	1.000	0.942	0.736	0.433	0.294	0.232	0.209	0.192	0.174	0.150	0.140	31.564	0.991119		
21	248A	2094.07	109.	114.	0.191	1.000	0.921	0.682	0.470	0.364	0.269	0.221	0.187	0.163	0.149	0.139	23.896	0.75033		
22	105A	2044.70	90.6	95.4	0.201	1.000	1.000	0.816	0.536	0.412	0.311	0.262	0.229	0.206	0.193	0.183	21.235	0.666768		
23	123A	2051.71	63.5	67.5	0.178	1.000	0.999	0.890	0.567	0.417	0.336	0.292	0.257	0.231	0.213	0.203	18.893	0.593239		
24	75A	2034.68	49.8	54.4	0.213	1.000	0.855	0.738	0.560	0.429	0.285	0.208	0.162	0.135	0.119	0.109	15.288	0.480052		
25	242A	2092.16	44.0	48.2	0.190	1.000	0.818	0.686	0.483	0.353	0.244	0.199	0.172	0.156	0.148	0.138	15.217	0.477804		
26	132A	2054.70	33.9	37.2	0.168	1.000	1.000	0.936	0.655	0.510	0.374	0.298	0.240	0.195	0.168	0.158	14.198	0.445815		
27	322A	2271.45	27.8	30.6	0.164	1.000	1.000	0.881	0.681	0.538	0.412	0.343	0.286	0.238	0.205	0.195	13.022	0.408879		
28	319A	2270.35	24.2	26.8	0.164	1.000	1.000	0.943	0.691	0.539	0.393	0.318	0.262	0.219	0.183	0.173	12.141	0.381229		
29	157A	2063.06	18.6	21.0	0.183	1.000	1.000	0.976	0.814	0.666	0.479	0.383	0.330	0.298	0.281	0.271	10.081	0.316543		
30	171A	2067.69	5.37	6.41	0.161	1.000	1.000	1.000	0.808	0.647	0.490	0.405	0.344	0.304	0.283	0.273	5.778	0.181416		
31	23A	2017.24	4.70	5.80	0.195	1.000	1.000	1.000	0.959	0.829	0.552	0.451	0.374	0.329	0.313	0.303	4.911	0.154202		



Swn

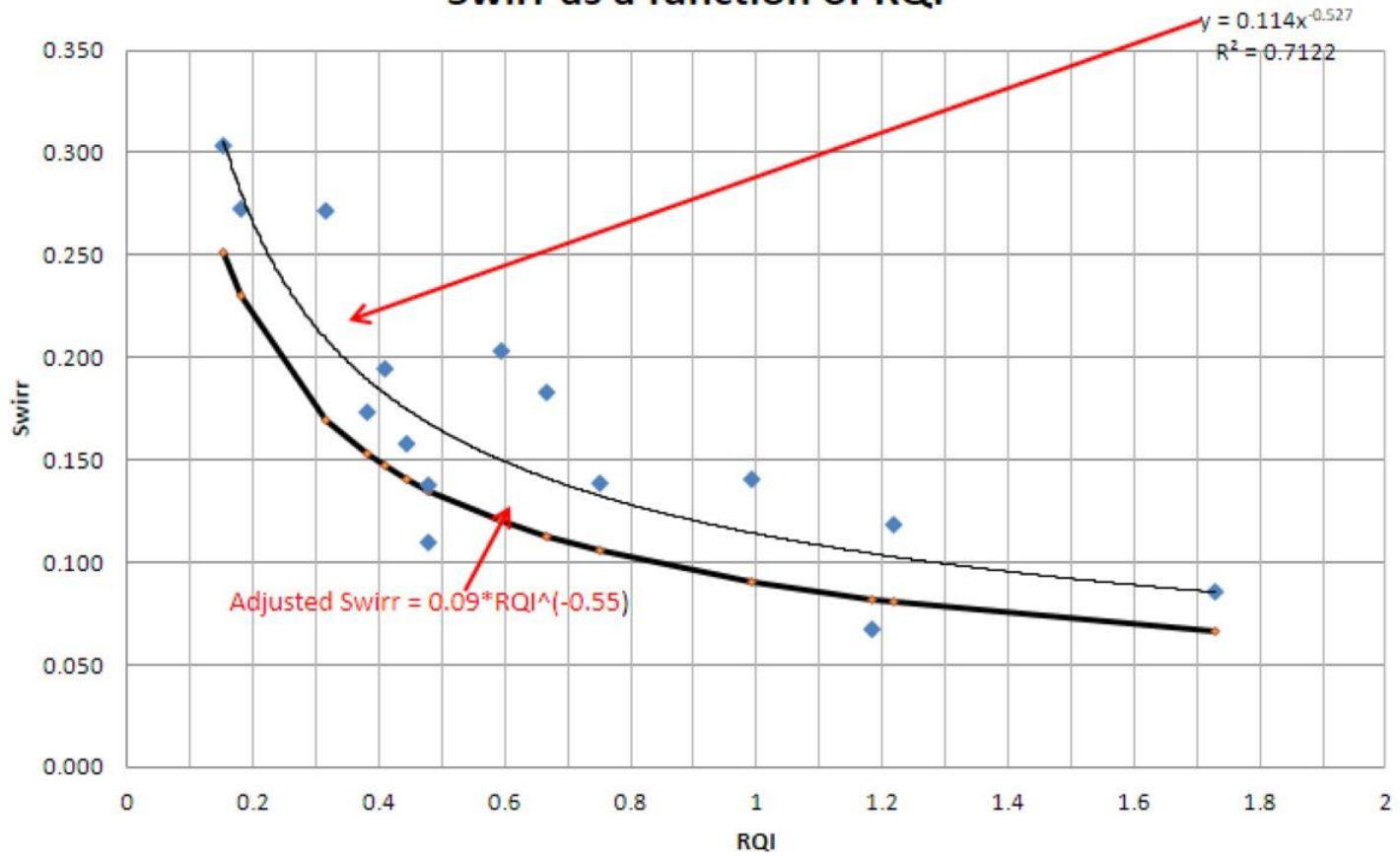
$$1. Sw_{irr} = 0.114 * RQI^{(-0.527)}$$

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	
9																					
10	All data		Pressure,			psi :	0	1	2	5	10	25	50	100	200	350					
11						HAFWL:		2.9	5.8	14.6	29.2	72.9	145.8	291.5	583.1	1020.4	ft				
12			Net Overburden (800 psi)																		
13	Sample	Depth	Klinkenberg	Permeability	Swn=Sw-Swir												Sqrt(k/Por)	RQI			
14	ID		Permeability	to air (est.)	Porosity												Swir			Swir_regression	
15		m	md	md	frac	frac Pore Volume															
16																					
17	196A	2076.47	685.	690.	0.226	0.907	0.588	0.498	0.335	-0.039	0.181	-0.053	-0.375	-4.717	2.619	0.086	55.1	1.729	0.0854		
18	91A	2040.02	332.	337.	0.220	0.886	0.758	0.717	0.356	-0.011	0.217	0.056	-0.140	-1.259	7.083	0.118	38.8	1.219	0.1027		
19	75A	2034.68	49.8	54.4	0.213	0.798	0.562	0.542	0.350	-0.013	0.183	0.101	0.024	-0.196	-0.774	0.109	15.3	0.480	0.1678		
20	89A	2039.36	211.	218.	0.212	0.871	0.813	0.736	0.433	0.025	0.232	0.104	-0.043	-0.730	-18.675	0.140	31.6	0.991	0.1145		
21	93A	2040.68	297.	305.	0.209	0.884	0.805	0.682	0.470	0.099	0.269	0.093	-0.106	-1.149	8.562	0.067	37.7	1.185	0.1043		
22	105A	2044.70	90.6	95.4	0.201	0.836	0.837	0.816	0.536	0.161	0.311	0.194	0.083	-0.263	-1.576	0.183	21.2	0.667	0.1411		
23	23A	2017.24	4.70	5.80	0.195	0.560	0.573	0.890	0.567	0.175	0.336	0.277	0.227	0.151	0.040	0.303	4.9	0.154	0.3053		
24	248A	2094.07	109.	114.	0.191	0.847	0.704	0.738	0.560	0.193	0.285	0.130	-0.006	-0.427	-2.438	0.139	23.9	0.750	0.1326		
25	242A	2092.16	44.0	48.2	0.190	0.798	0.618	0.686	0.483	0.118	0.244	0.151	0.071	-0.141	-0.696	0.138	15.2	0.478	0.1682		
26	157A	2063.06	18.6	21.0	0.183	0.736	0.741	0.936	0.655	0.286	0.374	0.267	0.175	0.016	-0.267	0.271	10.1	0.317	0.2090		
27	123A	2051.71	63.5	67.5	0.178	0.823	0.825	0.881	0.681	0.321	0.412	0.283	0.157	-0.159	-1.112	0.203	18.9	0.593	0.1501		
28	132A	2054.70	33.9	37.2	0.168	0.789	0.792	0.943	0.691	0.337	0.393	0.273	0.169	-0.052	-0.562	0.158	14.2	0.446	0.1745		
29	171A	2067.69	5.4	6.4	0.161	0.611	0.622	0.976	0.814	0.474	0.479	0.365	0.294	0.203	0.071	0.273	5.8	0.181	0.2803		
30	319A	2270.35	24.2	26.8	0.164	0.766	0.770	1.000	0.808	0.451	0.490	0.367	0.266	0.080	-0.293	0.173	12.1	0.381	0.1895		
31	322A	2271.45	27.8	30.6	0.164	0.777	0.780	1.000	0.959	0.633	0.552	0.410	0.289	0.086	-0.331	0.195	13.0	0.409	0.1826		

$$2. Swn = Sw - Sw_{irr}$$

Swirr

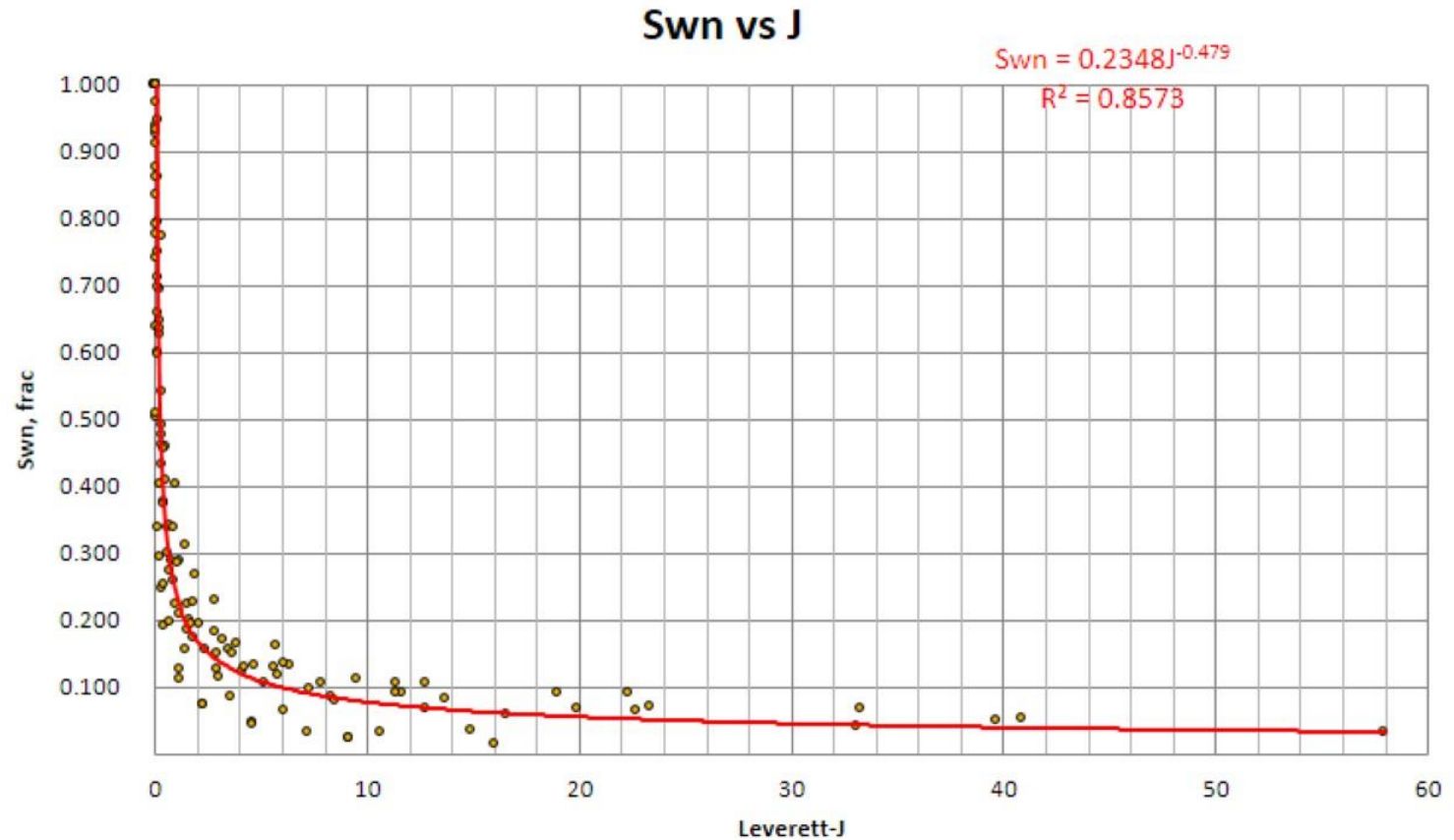
Swirr as a function of RQI



$$S_{wn} (=S_w - S_{wirr}) / (1 - S_{wirr})$$

		Pressure, psi :																
		0 1 2 5 10 25 50 100 200 350																
Sample ID	Depth	Net Overburden (800 psi)			S _{wn}													
		Klinkenberg Permeability	Permeability to air (est.)	Porosity	Pore Volume, frac											Sw _{ir final}	SQRT(k/Phi)	RQI
	m	md	md	frac														
196A	2076.47	685.	690.	0.226	1.000	0.659	0.462	0.287	0.200	0.122	0.084	0.058	0.041	0.031	0.067	55.063	1.729	
91A	2040.02	332.	337.	0.220	1.000	0.861	0.692	0.300	0.207	0.148	0.117	0.092	0.070	0.051	0.081	38.823	1.219	
93A	2040.68	297.	305.	0.209	1.000	0.740	0.501	0.292	0.192	0.111	0.074	0.047	0.023	0.082	37.725	1.185		
89A	2039.36	211.	218.	0.212	1.000	0.936	0.710	0.377	0.224	0.156	0.131	0.111	0.092	0.066	0.090	31.564	0.991	
248A	2094.07	109.	114.	0.191	1.000	0.912	0.645	0.408	0.289	0.183	0.129	0.091	0.065	0.049	0.105	23.896	0.750	
105A	2044.70	90.6	95.4	0.201	1.000	1.000	0.793	0.477	0.338	0.223	0.169	0.131	0.105	0.090	0.112	21.235	0.667	
123A	2051.71	63.5	67.5	0.178	1.000	0.999	0.876	0.508	0.338	0.246	0.196	0.156	0.126	0.106	0.120	18.893	0.593	
75A	2034.68	49.8	54.4	0.213	1.000	0.833	0.697	0.491	0.340	0.173	0.085	0.031		0.135	15.288	0.480		
242A	2092.16	44.0	48.2	0.190	1.000	0.790	0.637	0.402	0.252	0.126	0.073	0.043	0.024	0.015	0.135	15.217	0.478	
132A	2054.70	33.9	37.2	0.168	1.000	1.000	0.925	0.599	0.430	0.271	0.183	0.115	0.064	0.032	0.140	14.198	0.446	
322A	2271.45	27.8	30.6	0.164	1.000	1.000	0.860	0.626	0.458	0.311	0.229	0.162	0.106	0.068	0.147	13.022	0.409	
319A	2270.35	24.2	26.8	0.164	1.000	1.000	0.932	0.635	0.455	0.284	0.194	0.129	0.078	0.036	0.153	12.141	0.381	
157A	2063.06	18.6	21.0	0.183	1.000	1.000	0.971	0.776	0.598	0.373	0.257	0.193	0.155	0.134	0.169	10.081	0.317	
171A	2067.69	5.37	6.41	0.161	1.000	1.000	1.000	0.750	0.542	0.337	0.227	0.148	0.096	0.068	0.230	5.778	0.181	
23A	2017.24	4.70	5.80	0.195	1.000	1.000	1.000	0.945	0.771	0.402	0.266	0.163	0.104	0.082	0.252	4.911	0.154	

Swn expressed as a function of J

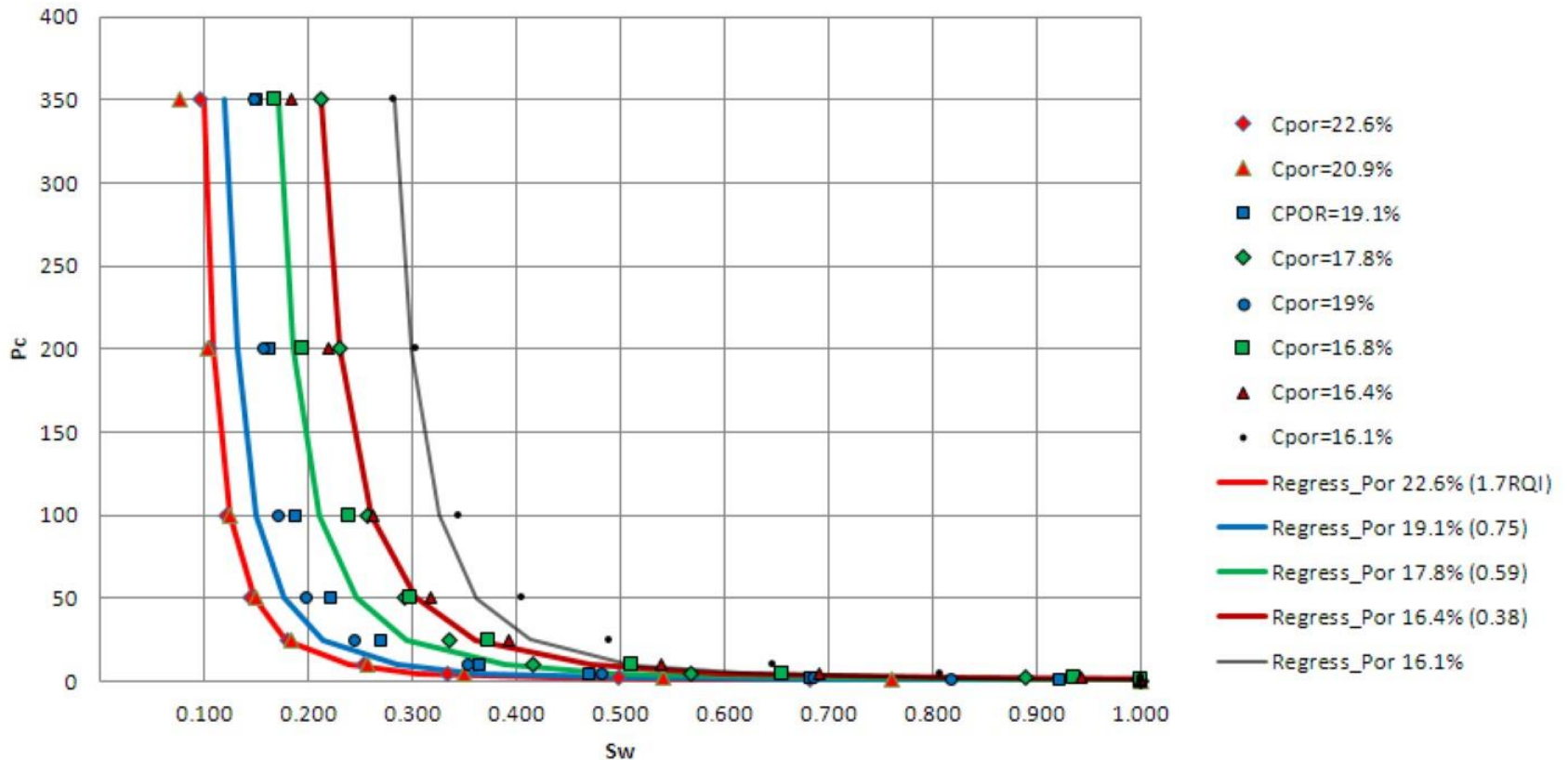


Final equations

- $S_{wn} = 0.2348 * J^{(-0.47)} \dots\dots\dots(1)$
- $J = 0.2166 * P_c * \sqrt{K/\phi} / \sigma \cos\theta \dots\dots\dots(2)$
- $\sigma \cos\theta = 72 \text{ dynes/cm} \dots\dots\dots(3)$
- $S_{wn} = 0.2348 * [0.003 * P_c * \sqrt{K/\phi}]^{(-0.47)}$
- $\quad = 3.596 * [P_c * \sqrt{K/\phi}]^{(-0.47)}$
- $S_{wirr} = 0.09 * RQI^{(-0.55)}$
 $\quad = 0.6038 * \sqrt{K/\phi}^{(-0.55)} \dots\dots\dots(4)$
- $S_w = S_{wn} * (1 - S_{wirr}) + S_{wirr}$
- $S_w = 3.596 * [P_c * \sqrt{K/\phi}]^{(-0.47)} * (1 - 0.604 * \sqrt{K/\phi}^{(-0.55)}) + 0.604 * \sqrt{K/\phi}^{(-0.55)} \dots\dots\dots(5)$

Final Test of the SH_Function

Overlay SW_J over SW_capP (original)



The SH_Function discussed above are at laboratory conditions. For reservoir condition, $T\cos\phi = 50$ dynes/cm should be used instead of 72 dynes/cm in the final equation.

Conversion to Reservoir conditions

$$\frac{P_{cL}}{P_{cR}} = \frac{(T \cos\theta)_L}{(T \cos\theta)_R}$$

$$\therefore P_{cR} = P_{cL} \cdot \frac{(T \cos\theta)_R}{(T \cos\theta)_L}$$

For air-brine system, $P_{cR} = P_{cL} * 50/72$

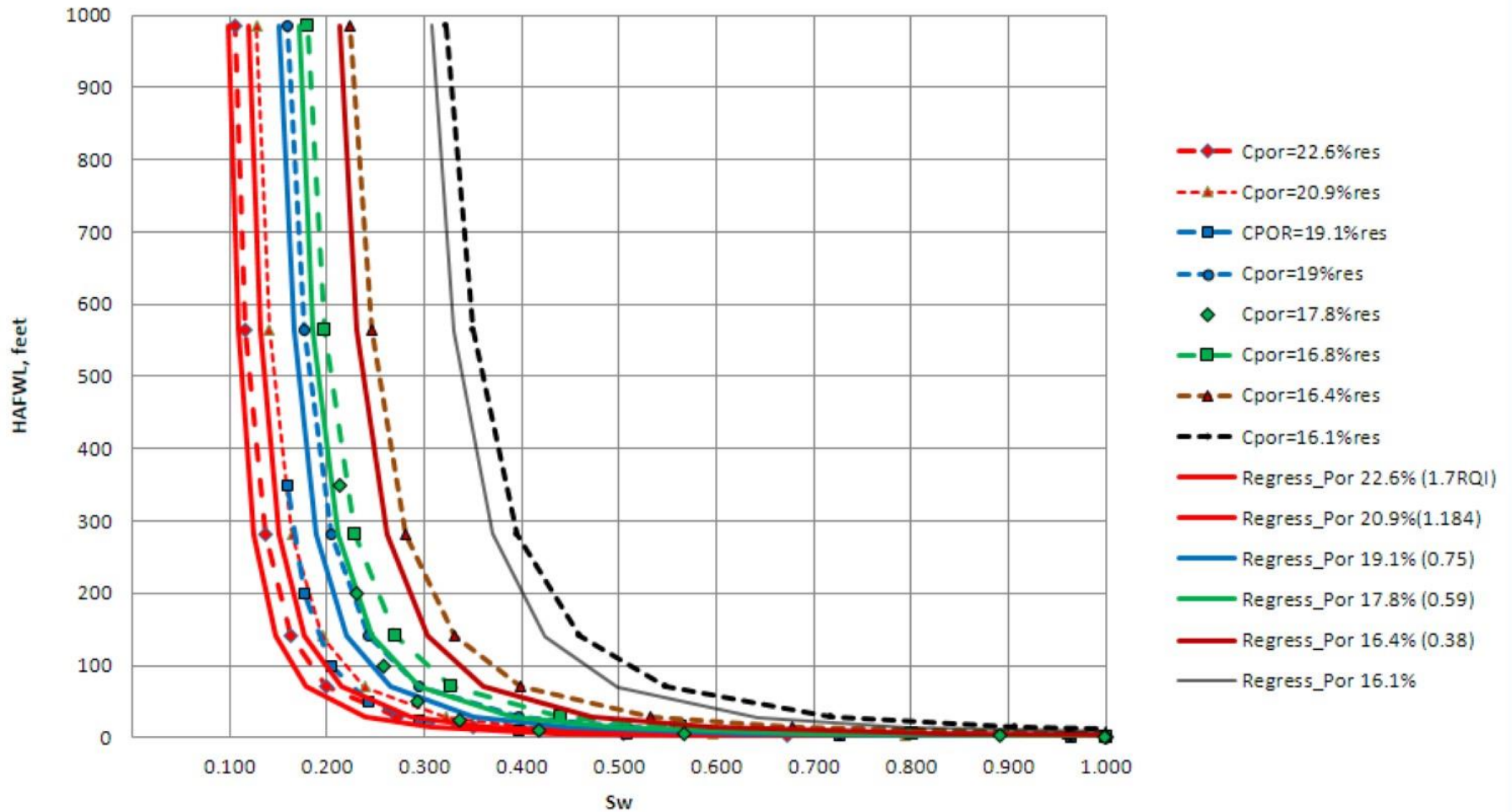
Final equations at reservoir conditions

- $S_w = 3.596 * [P_c * \sqrt{K/\phi}]^{-0.47} * (1 - 0.604 * \sqrt{K/\phi}^{-0.55}) + 0.604 * \sqrt{K/\phi}^{-0.55} \dots (5)$
- $S_w(\text{res}) = 3.596 * [P_c * (50/72) * \sqrt{K/\phi}]^{-0.47} * (1 - 0.604 * \sqrt{K/\phi}^{-0.55}) + 0.604 * \sqrt{K/\phi}^{-0.55} \dots (6)$
- $S_{w_res} = 3.596 * [(P_{\text{water}} - P_{\text{Gas}}) * H * (50/72) * \sqrt{K/\phi}]^{-0.47} * (1 - 0.604 * \sqrt{K/\phi}^{-0.55}) + 0.604 * \sqrt{K/\phi}^{-0.55} \dots (7)$

where H is the height above free water level in feet and P_{water} and P_{gas} are in psi/ft.

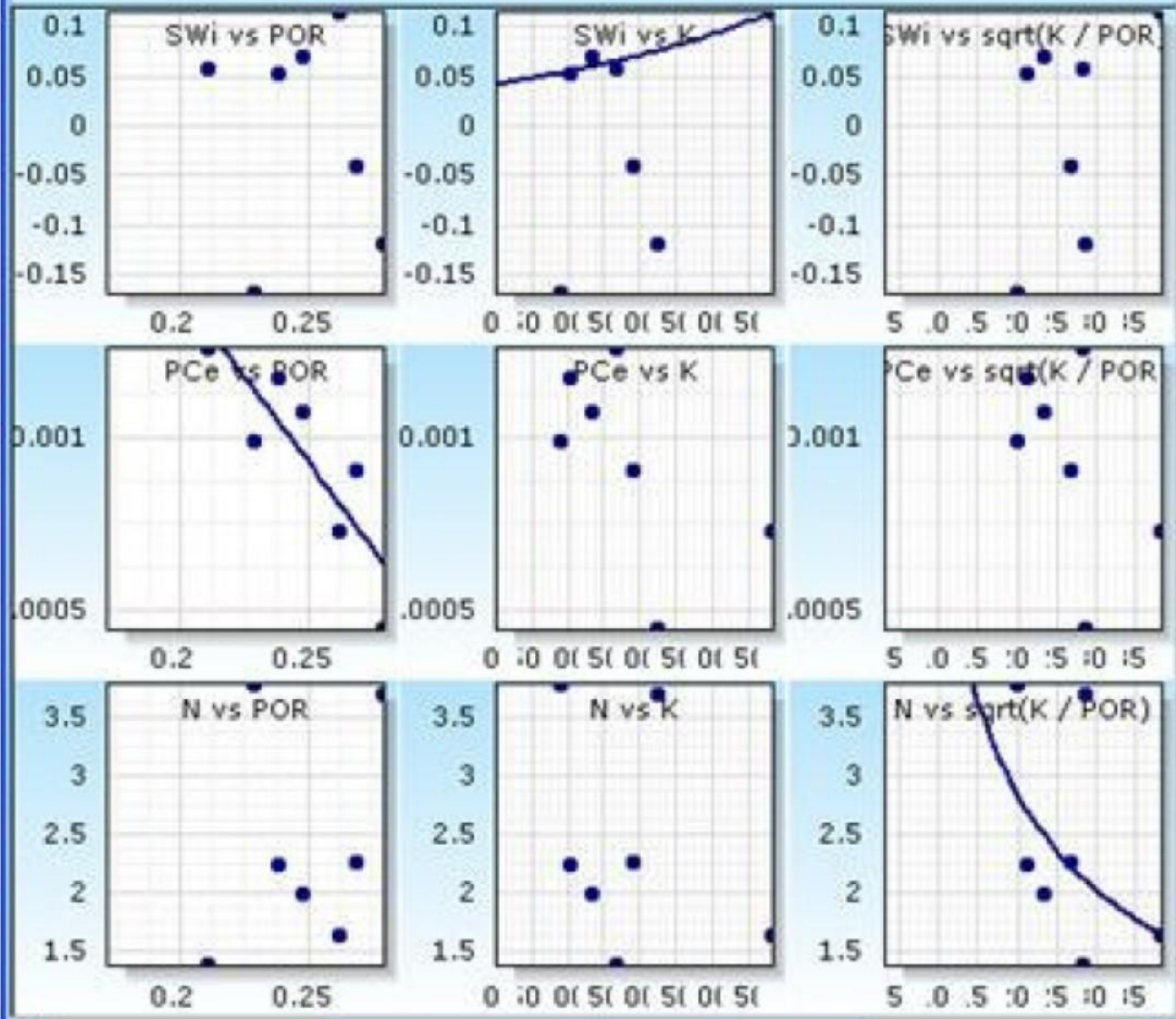
Comparison of SW_J(res) with SW_J(lab)

Overlay SW_J (res) vs SW_J(lab)



Thank you for your patience

Relationship between the parameters and the input variables



Number of regressions to investigate

The different regressions are:

1. Linear $P = C_1 + C_2 * INPUT$
2. Logarithmic $P = C_1 + C_2 * \log_{10}(INPUT)$
3. Power $P = C_1 * pow(INPUT, C_2)$
4. Exponential $P = pow_{10}(C_1 + C_2 * INPUT)$